# Removal and recovery of NO by MnO<sub>2</sub>/Mg-Al layered double hydroxide

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### **INTRODUCTION**

The incineration of waste generates exhaust gas containing poisonous nitrogen oxides (NO<sub>x</sub>). At present, Selective Catalytic Reduction (SCR) process is used for NO<sub>x</sub> removal. But treated product cannot be recycled and the high maintenance cost also become issue. Because of their capable of gas recovery and low price,  $CO_3 \cdot Mg$ -Al layered double hydroxides (LDHs) has considerable attention in recent years. From anion exchange ability, they are used as adsorbent for nitrogen dioxide (NO<sub>2</sub>) removal, and adsorbed gases can be recovered in wet process<sup>1</sup>). However, they cannot remove nitric oxide (NO) contained more than 95 percent of NOx in exhaust gas<sup>1</sup>). Therefore, NO must be oxidized to NO<sub>2</sub> for removal. Transition metal oxides have high performances in NO oxidation. Mn based composite oxides are less expensive compared with others, and it has high activity in NO oxidation<sup>2</sup>). In this study, we investigated the performance of NO treatment by MnO<sub>2</sub>/Mg-Al LDH composite and MnO<sub>2</sub> + CO<sub>3</sub> · Mg-Al LDH mixture compared with CO<sub>3</sub> · Mg-Al LDH<sup>3-5</sup>). Additionally, NO removed by MnO<sub>2</sub>/Mg-Al LDH was examined to recover by thermal treatment.

### MATERIALS AND METHODS

#### Preparation of MnO<sub>2</sub>/Mg-Al LDH

 $CO_3 \cdot Mg$ -Al LDH (Mg/Al molar ratio = 2) was synthesized through co-precipitation and calcined at 500 °C for 2 h to yield Mg-Al oxide. Mg-Al oxide was added to KMnO<sub>4</sub> solution adjusted to Mn/Al molar ratios of 5 and stirred at 300 rpm and 30 °C. N<sub>2</sub> was bubbled into the solution throughout the procedure. After stirring for 6 h, solids were separated from the liquid and dried at 40 °C for 24 h, and MnO<sub>2</sub>/Mg-Al LDH was obtained. MnO<sub>2</sub>/Mg-Al LDH was analyzed by using X-ray diffraction (XRD), inductively coupled plasma-atomic emission spectrometry (ICP-AES), X-ray photoelectron spectroscopy (XPS).

#### **NO treatment**

 $MnO_2/Mg$ -Al LDH composite,  $MnO_2 + CO_3 \cdot Mg$ -Al LDH mixture, or  $CO_3 \cdot Mg$ -Al LDH were packed in reaction tube preheated to 170°C by electric tuber furnace. The mixed gas (NO: 150 ppm O<sub>2</sub>: 10%, N<sub>2</sub>: balance) was passed through the adsorbent for 90 min, with the flow rate adjusted by the mass flow controller (linear velocity 1.0 m/min). The residual concentrations were analyzed using a gas analyzer.

# **NO** recovery

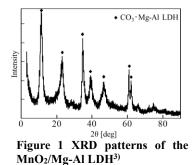
NO removed by MnO<sub>2</sub>/Mg-Al LDH was recovered by thermal treatment. Firstly, desorbed temperature was analyzed via Evolved gas analysis-mass spectrometry (EGA-MS). MnO<sub>2</sub>/Mg-Al LDH had 1.33 mmol/g of NO,

and the materials were treated at 400-600°C using the above-mentioned apparatus.

# **RESULTS AND DISCUSSION**

### Preparation of MnO<sub>2</sub>/Mg-Al LDH

Figure 1 and Table 1 show the XRD patterns of the  $MnO_2/Mg$ -Al LDH, and its chemical compositions. The XRD patterns indicate that LDH structure presents in the sample, while Mn species was not observed. But it contained 4.2 wt% of Mn, and basal spacing,  $d_{003}$ , was 7.6 Å. This suggests that  $MnO_4^-$  was intercalated between the LDH layers. XPS analysis indicates that 76.7% of the Mn was Mn (IV).  $MnO_4^-$ , intercalated between the LDH layers, was probably reduced to  $MnO_2$  in the interlayer.

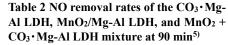


#### **NO treatment**

Table 2 shows the NO removal rates of the  $CO_3 \cdot Mg$ -Al LDH, MnO<sub>2</sub>/Mg-Al LDH, and MnO<sub>2</sub> + CO<sub>3</sub> · Mg-Al LDH mixture. After 90 min, the NO removal rates of CO<sub>3</sub> · Mg-Al LDH, MnO<sub>2</sub>/Mg-Al LDH, and MnO<sub>2</sub> + CO<sub>3</sub> · Mg-Al LDH mixture are 0%, 1.4%, and 83.9% respectively. The NO removal rates of MnO<sub>2</sub>/Mg-Al LDH is notably higher than the others, indicating that a synergistic effect was generated when it becomes composite.

#### Table 1 Chemical compositions of MnO<sub>2</sub>/Mg-Al LDH<sup>4)</sup>

Mg/Al	Mn [wt%]	Mn/Al	CO32-/Al	OH-/Al
1.9	4.2	0.19	0.28	0.43



	CO <sub>3</sub> · Mg-Al LDH	MnO <sub>2</sub> /Mg-Al LDH		MnO <sub>2</sub> + CO <sub>3</sub> ·Mg-Al LDH mixture			
NO removal rate [%]	0	1.4		100			
Table 3 NO recovery							
		400°C	500°	C 600°C			
Recovery	rate [%]	1.0	46.2	2 100			

### **NO** recovery

EGA-MS result of  $MnO_2/Mg$ -Al LDH after NO removal shows Recovery rate [%] 1.0 46.2 100 that NO peak was observed over 400 °C. NO recovery at 400-600 °C are shown in table 3. NO recovery performed at 600 °C presents 100% of recovery rate that significantly higher than 500 °C and 400 °C.

# CONCLUSION

NO treatment by MnO<sub>2</sub>/Mg-Al LDH composite has higher performance than  $CO_3 \cdot Mg$ -Al LDH and MnO<sub>2</sub> +  $CO_3 \cdot Mg$ -Al LDH mixture and denote 83.9% of removal rate. Moreover, trapped NO gas can be recovered 100 % at 600 °C.

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